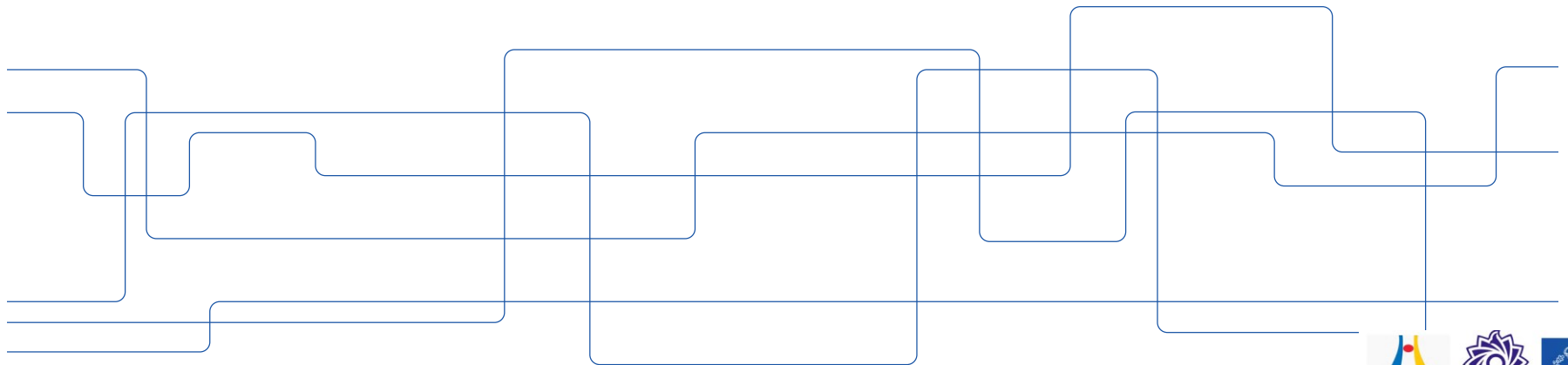




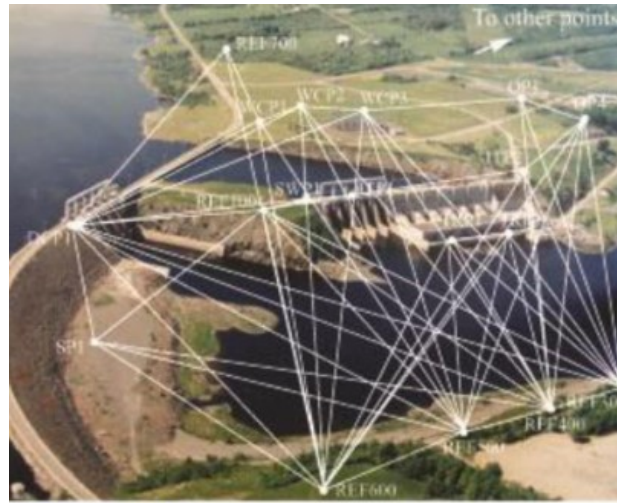
# A new approach for reducing physical and geometric effects in small-scale geodetic control networks

**Mohammad Bagherbandi**, Masoud Shirazian, Jonas Ågren, Milan Horemuz, Hamed Karimi



# Classical geodetic control network

- One of the primary issues of geodesy is the building and maintenance of small-scale precise geodetic control networks of which the longest baseline lengths are a few kilometers. e.g.
  - To monitor the deformation or deflection in dams
  - Tunnels
  - High towers
  - Landslide



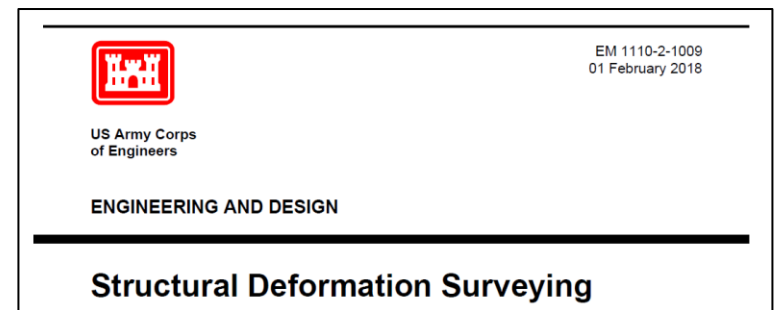
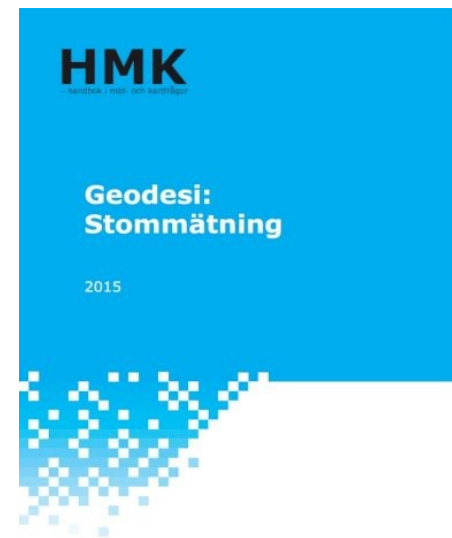
- **Challenges**
  - Refraction error,
  - Geometric effects (Curvature-skewness)
  - Physical effects (Deflection of the verticals)
- **Reducing slope to horizontal distances is a challenges for us** (without involving any systematic error)

} **These problems influence zenith angles**

Is it possible to avoid reading vertical angles?

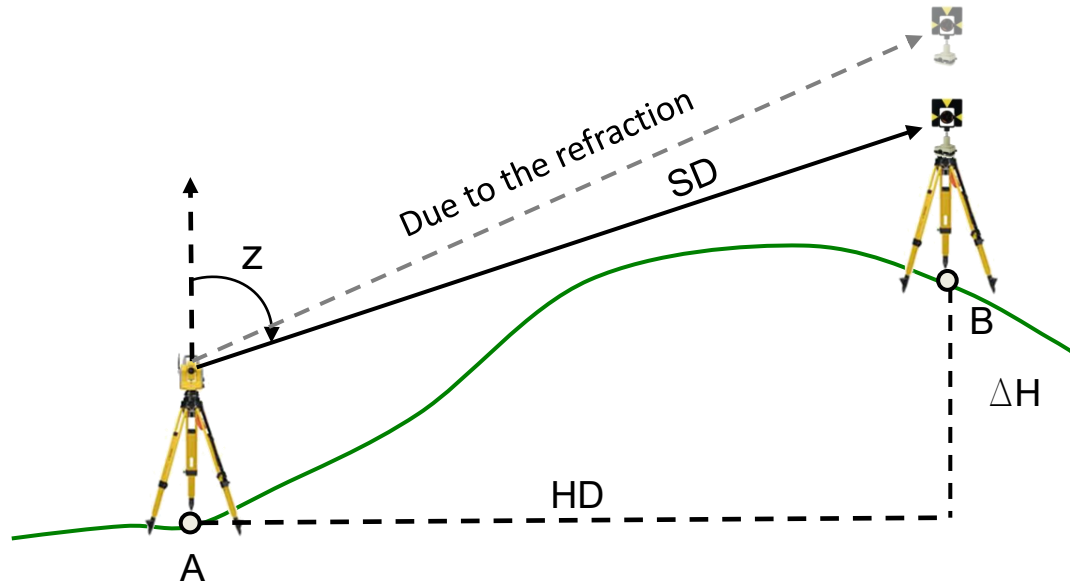
# Aim

To quantify the physical and geometric effects (assuming a **spherical** and **ellipsoidal** Earth model) on the vertical angles by performing a simulation that can be relevant and useful for the writing of surveying guidelines.



**These problems have not been clearly mentioned in the guidelines.**

# Reduction of slope distance to horizontal distance in the geodetic networks: **Refraction error**

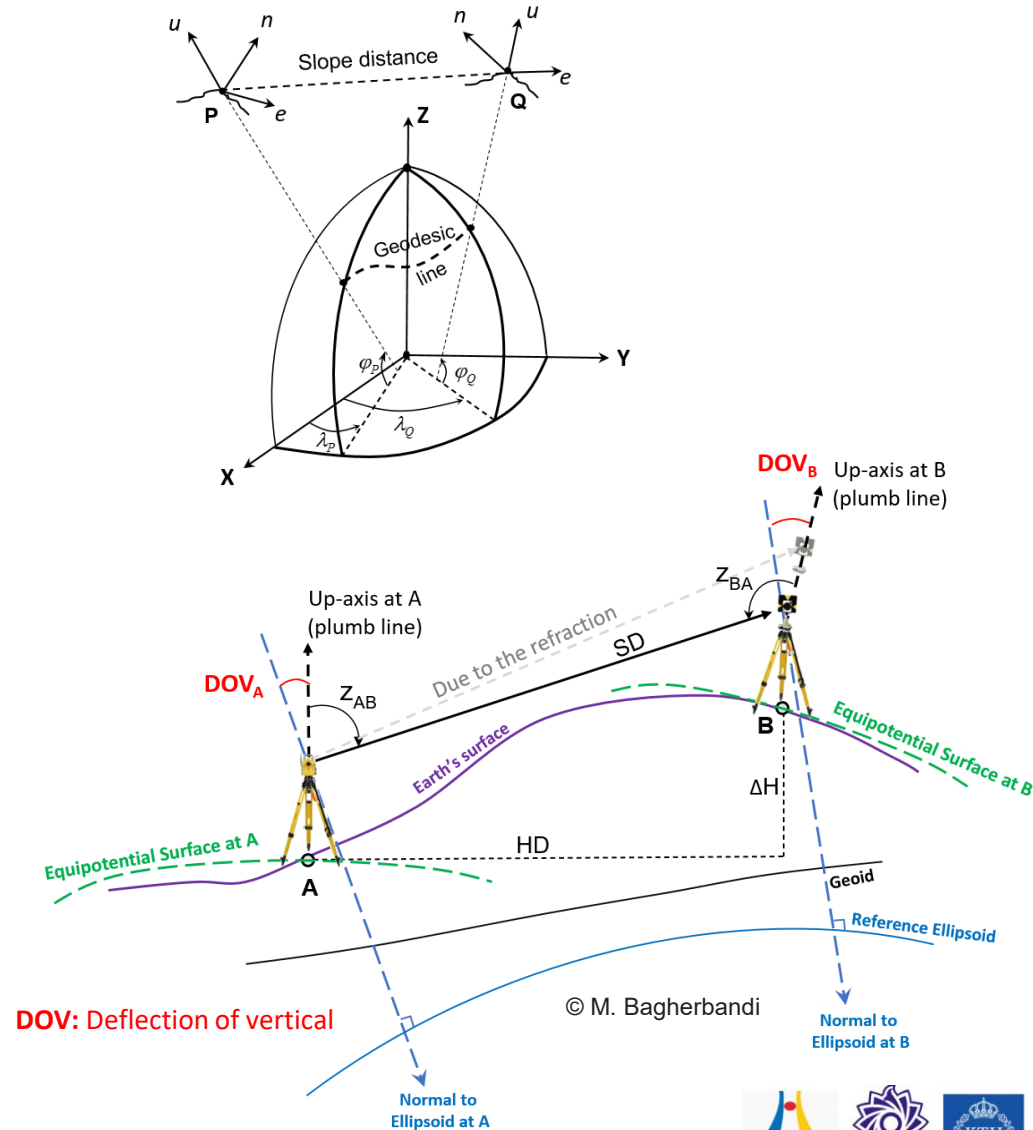


$$HD = SD \cos(90 - Z) = SD \sin Z$$

- The refraction is caused by variations in the air density
- Refraction causes objects (located far away) seem to be higher than they actually do
- Positive correction
- In that case, the measured zenith distance becomes too small.
- **A negative correction is required or reciprocal reading**

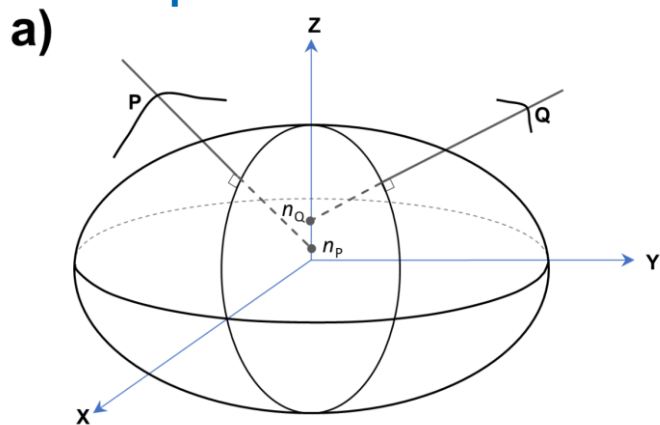
# Reduction of slope distance to horizontal distance in the geodetic networks: physical and geometric problems

- Definition of a proper coordinate system is one of the most important problems in establishing of a classical geodetic network.
- The common practice is to establish either
  - a local geodetic or
  - local astronomic coordinate system
- The physical and geometric problems occur when the up-component directions (i.e. plumb line or normal direction) are different at the start and end points of a baseline.

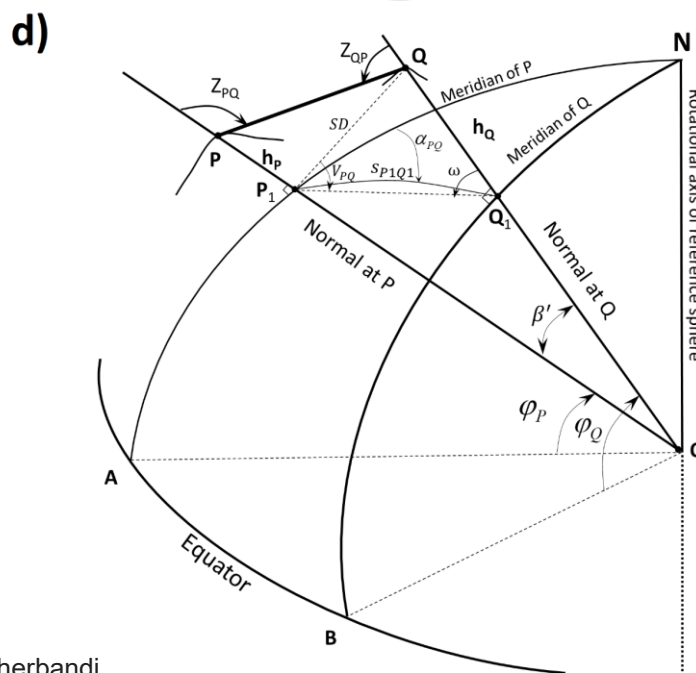
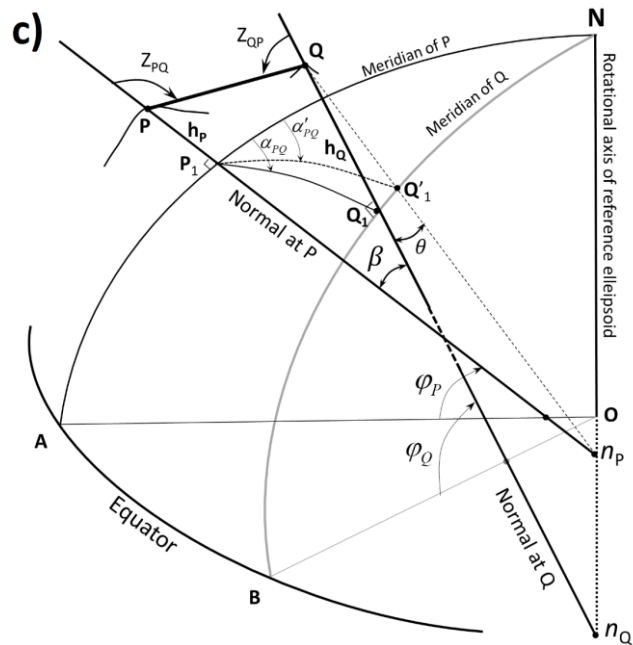
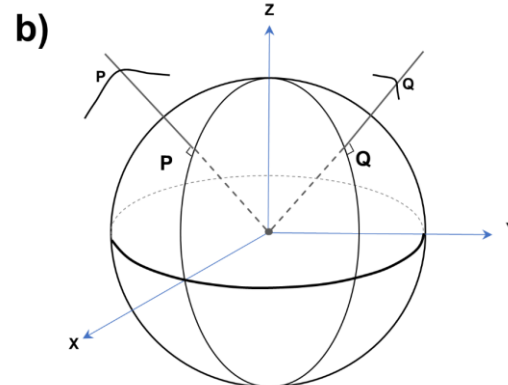


# Curvature-skewness problem ellipsoidal vs spherical model

## Ellipsoidal model



## Spherical model



© M. Bagherbandi

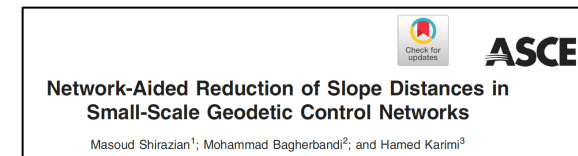
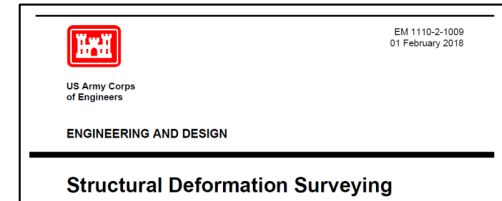
# Solutions for the challenges

## ■ Challenges

- Refraction error,
- Geometric effects (curvature-skewness)
- Physical effects (Deflection of the verticals → DOV)

## ■ Solutions:

- Refraction error: the recommended solution to solve this problem is the reciprocal reading of vertical angles at the same time from both ends of a distance (Engineer manual 2018, Section 3-4)
- Reciprocal reading can be a solution for geometric and physical effects, if the points are **at the same elevation**. Otherwise:
  - Curvature-skewness error should be taken into account for correcting vertical angles.
  - The DOV affects the collected zenith angles should be used for converting slope distances to horizontal distances.
    - Using regional gravity database and calculating precise DOV components (i.e.  $\zeta$ ,  $\eta$ ) and correcting the geodetic observations.
- Network-aided method (J. Surv. Eng., 2021, 147(4): 04021024).



### Note:

Collecting reciprocal observations is **time-consuming**, especially in the rough topography areas (e.g. dam sites) and increases the fieldwork and costs of the projects. **Cost and time** are important factors to establish optimum and precise geodetic networks (Kuang 1996).

# Quantifying physical (DOV) and Curvature- skewness errors on the reduction of slope distance to horizontal distance

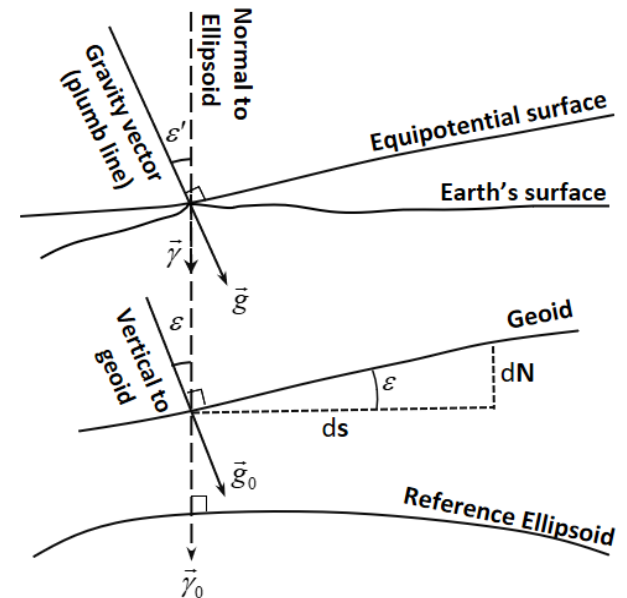


# Deflection of vertical (DOV)

- The DOV components at the Earth's surface using the quasigeoid and Molodenskij's definition of the height anomaly. Molodensky et al. (1962) discarded the geoid and defined a new surface, the quasigeoid, in which the geoidal undulation is replaced by height anomaly (Heiskanen and Moritz 1967, p. 312):

$$\text{North-south component} \quad \xi' = -\frac{1}{R} \frac{\partial \zeta}{\partial \varphi} - \frac{\Delta g}{\gamma} \frac{1}{R} \frac{\partial H}{\partial \varphi}$$

$$\text{East-west component} \quad \eta' = -\frac{1}{R \cos \varphi} \frac{\partial \zeta}{\partial \lambda} - \frac{\Delta g}{\gamma} \frac{1}{R \cos \varphi} \frac{\partial H}{\partial \lambda}$$



## Data:

- SWEN17\_RH2000 → is a quasigeoid model
- The terrain inclinations are derived using the Swedish photogrammetric DEM (second terms).

# Effect of DOV on horizontal distances

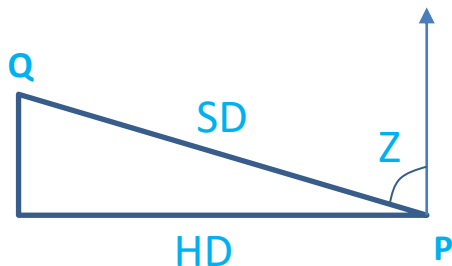
- Effect of DOV on zenith angle

$$\delta_{Z_P} = \xi'_P \cos(\alpha_{PQ}) + \eta'_P \sin(\alpha_{PQ})$$

- Coverting slope distance to horizontal distance

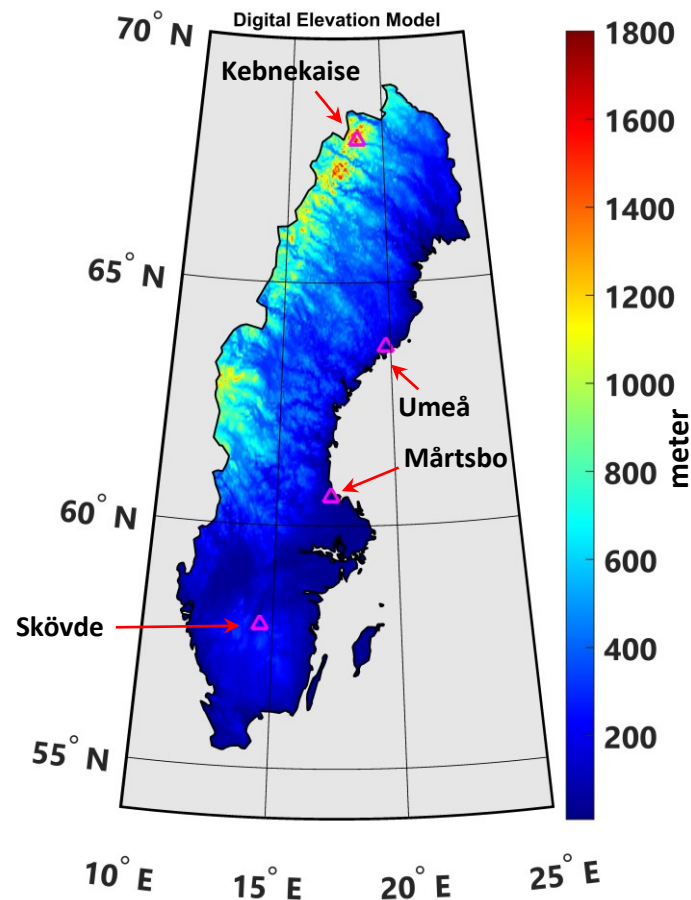
$$HD = SD \cos(90 - Z) = SD \sin Z$$

- HD: horizontal distance
- SD: Slope distance
- Z: Zenith (vertical) angle



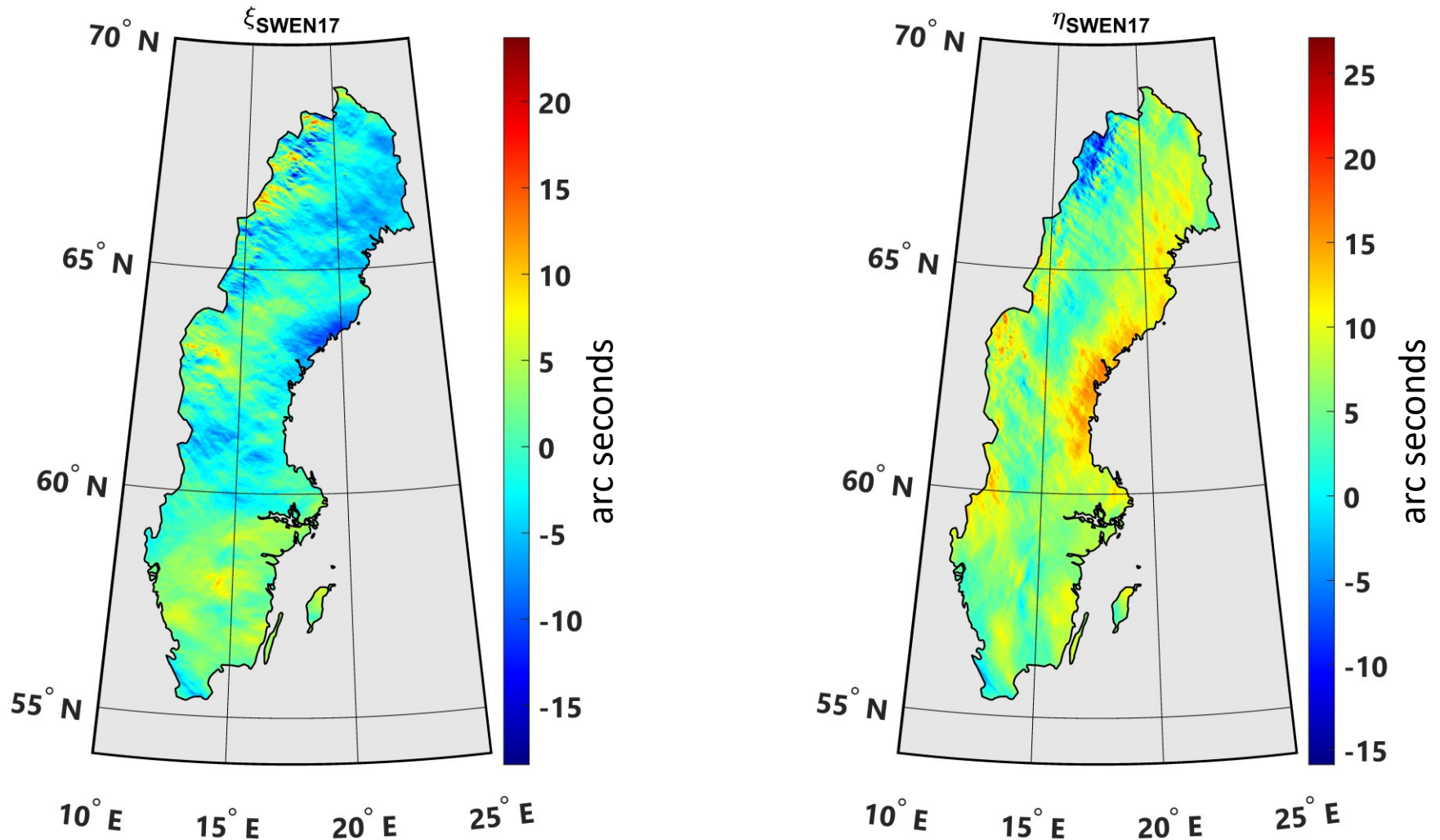
- Variation of HD due to the effect of DOV on Zenith angle:

$$\delta_{HD} = SD \sin(Z + \delta_{Z_P}) - SD \sin(Z)$$



Location	Latitude	Longitude	Height (m)
Kebnekaise	67.93° N	18.60° E	1702.3
Umeå	63.68° N	19.78° E	84.0
Märtsbo	60.595143° N	17.258525° E	32.1
Skövde	57.95° N	14.50° E	262

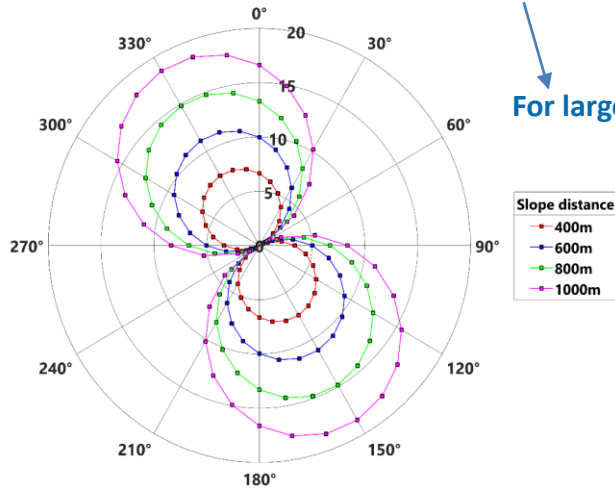
# Results: DOV components at the Earth's surface



The resolution of the DOV components in latitude and longitude directions are  $0.01^\circ$  and  $0.02^\circ$

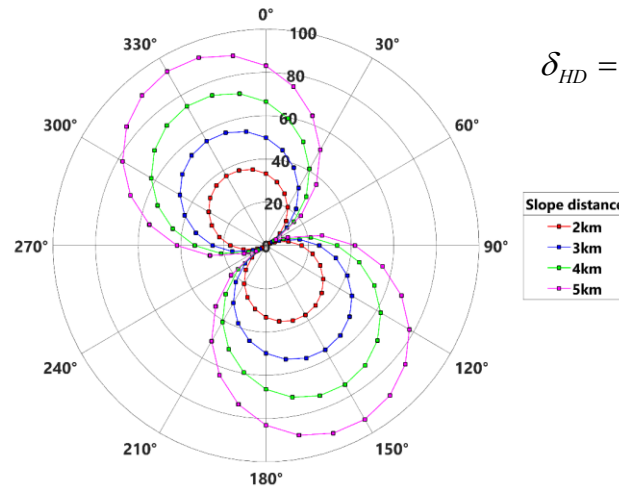
# Effect of DOV on horizontal distances: Kebnekaise

Effect of DOV on horizontal distance  $|\delta_{HD}|$  in mm (zenith angle=70°)



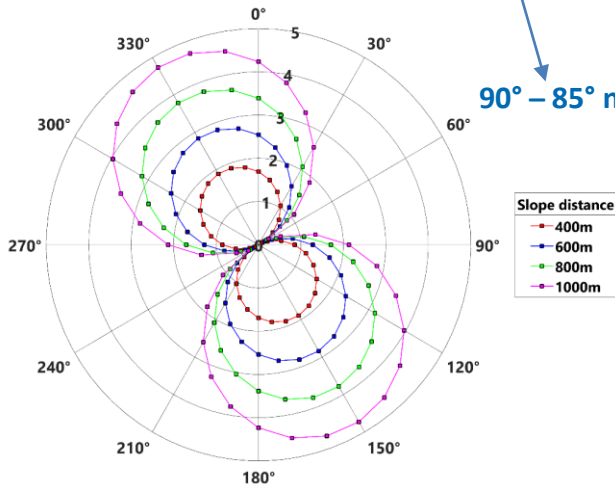
For larger  $\Delta H$

Effect of DOV on horizontal distance  $|\delta_{HD}|$  in mm (zenith angle=70°)



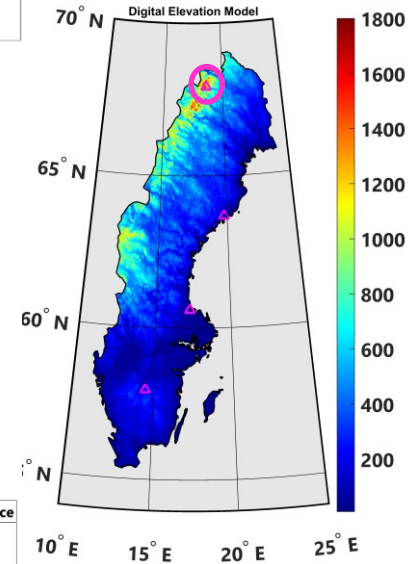
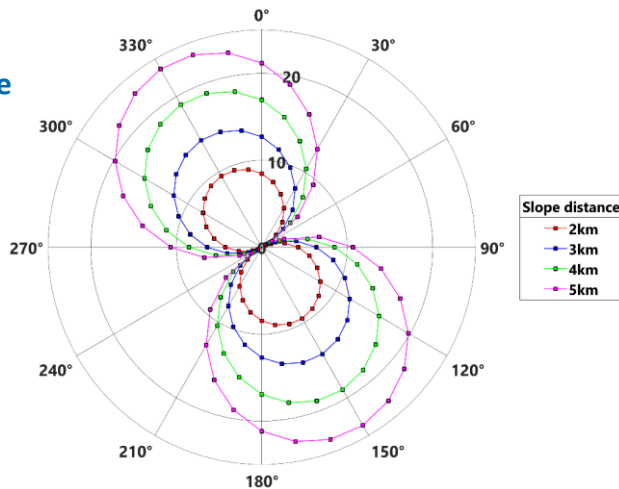
$$\delta_{HD} = SD \sin(Z + \delta_{Z_p}) - SD \sin(Z)$$

Effect of DOV on horizontal distance  $|\delta_{HD}|$  in mm (zenith angle=85°)



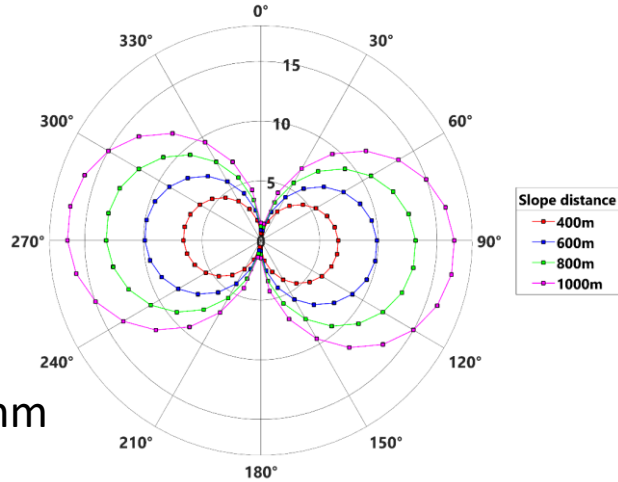
90° – 85° normal case

Effect of DOV on horizontal distance  $|\delta_{HD}|$  in mm (zenith angle=85°)



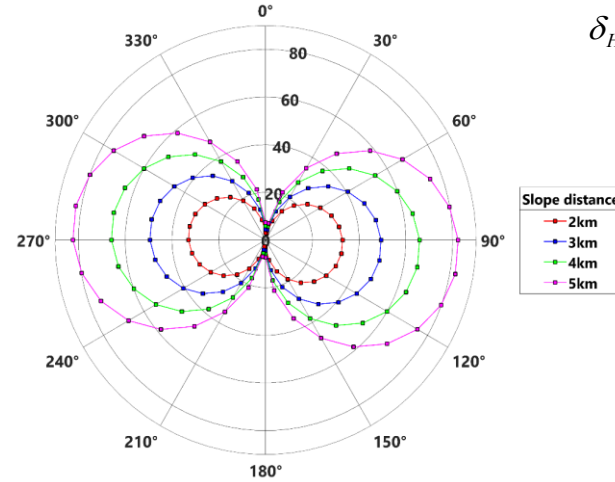
# Effect of DOV on horizontal distances: Mårtsbo

Effect of DOV on horizontal distance  $|\delta_{HD}|$  in mm (zenith angle=70°)



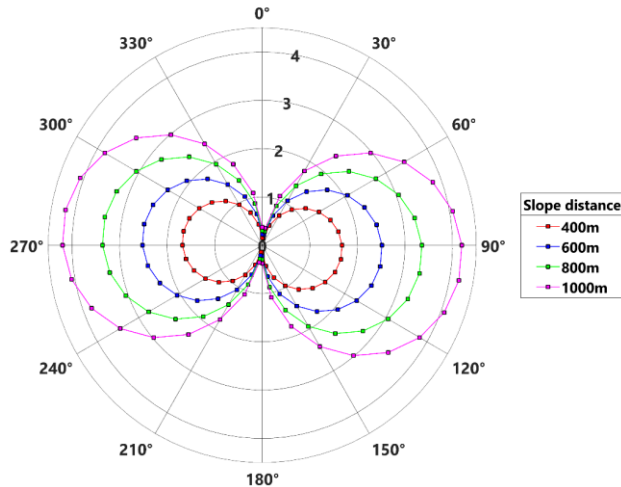
1 km  
16.5 mm

Effect of DOV on horizontal distance  $|\delta_{HD}|$  in mm (zenith angle=70°)



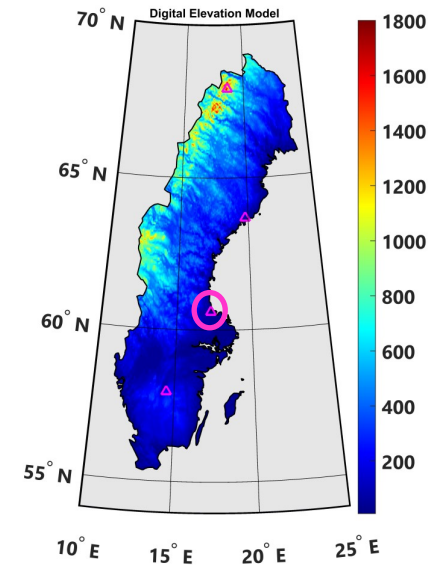
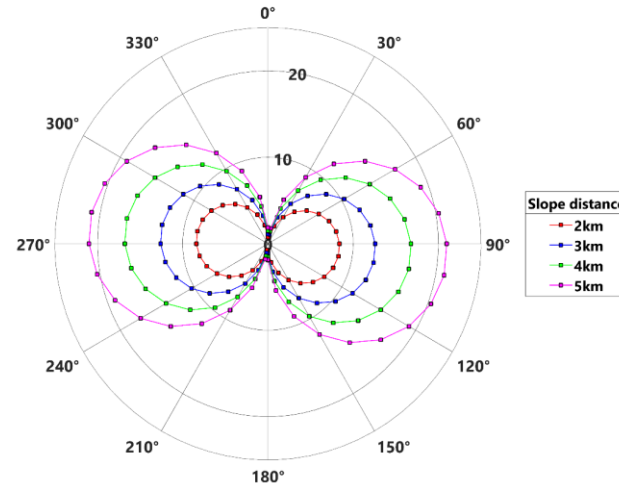
$$\delta_{HD} = SD \sin(Z + \delta_{Z_p}) - SD \sin(Z)$$

Effect of DOV on horizontal distance  $|\delta_{HD}|$  in mm (zenith angle=85°)



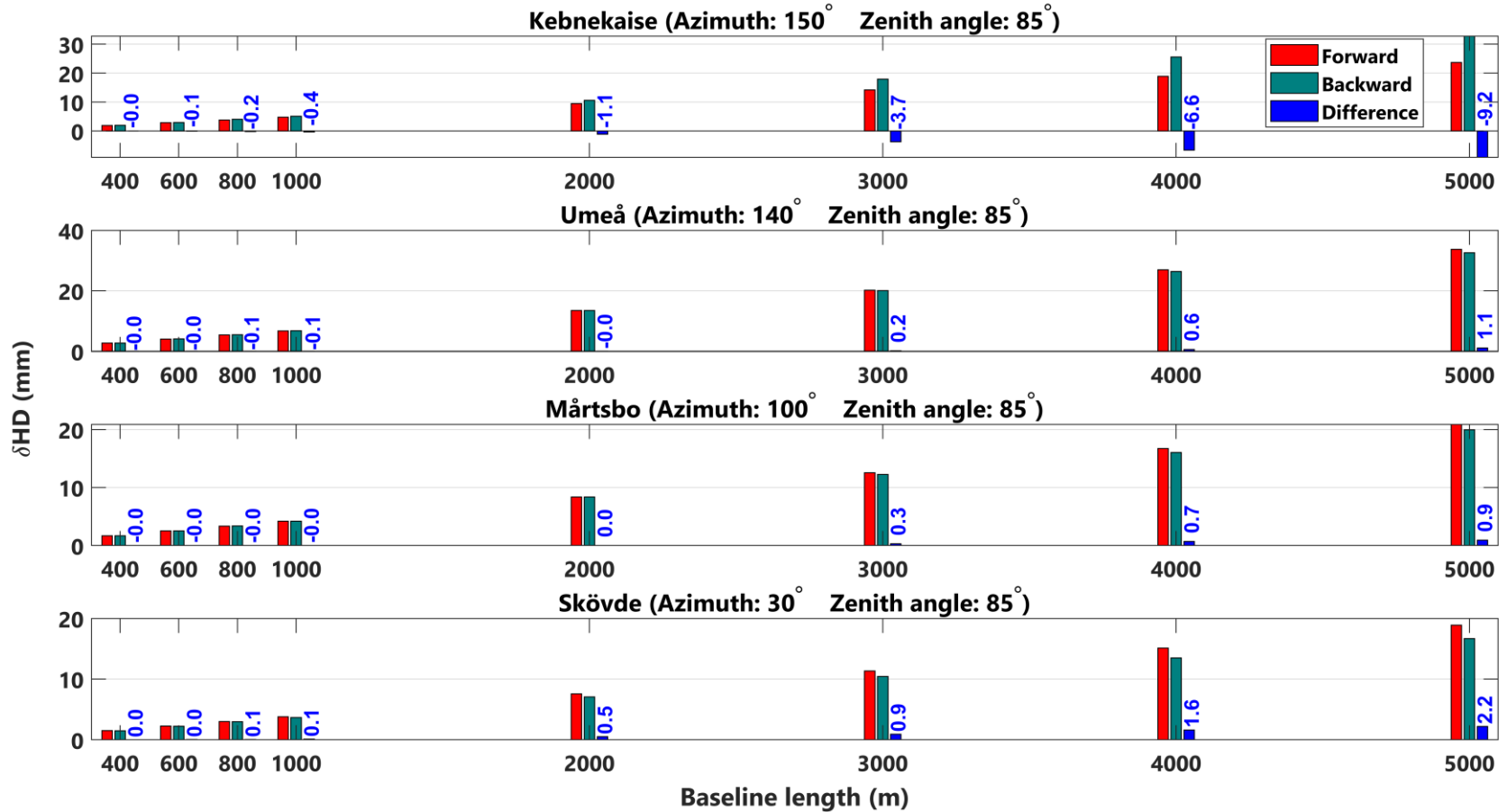
1 km  
4.2 mm

Effect of DOV on horizontal distance  $|\delta_{HD}|$  in mm (zenith angle=85°)



# Forward and Backward DOV effect on the horizontal distances for different baselines

$$\delta_{HD} = SD \sin(Z + \delta_{Z_p}) - SD \sin(Z)$$



The impact of DOV on forward and backward measurements is almost the same if the height difference between start- and end-points are small ( $\Delta H < 50$  m).

# How to calculate the curvature-skewness effect on slope distance reduction?

# Curvature-skewness effect on horizontal distance on an ellipsoid

- Forward slope angle (from P to Q)

–  $(\varphi, \lambda)_P \xrightarrow[\text{algorithm}]{\text{Vincenty's}} (\varphi, \lambda)_Q \rightarrow (e, n)_P \text{ and } (e, n)_Q$

$$V_{PQ} = V = \tan^{-1} \left( \frac{\Delta u_{PQ}}{\sqrt{\Delta e_{PQ}^2 + \Delta n_{PQ}^2}} \right)$$

- Backward slope angle (from Q to P)

–  $(\varphi, \lambda)_Q \xrightarrow[\text{algorithm}]{\text{Vincenty's}} (\varphi, \lambda)_P \rightarrow (e, n)_P \text{ and } (e, n)_Q$

$$V_{QP} = V + \beta = \tan^{-1} \left( \frac{\Delta u_{QP}}{\sqrt{\Delta e_{QP}^2 + \Delta n_{QP}^2}} \right)$$

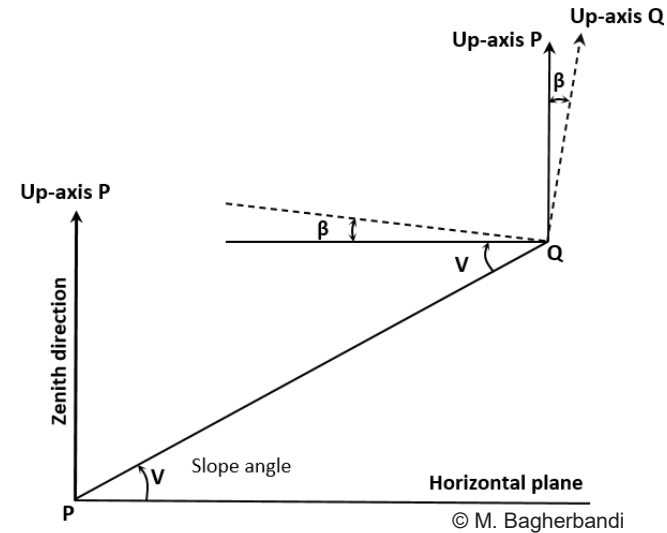
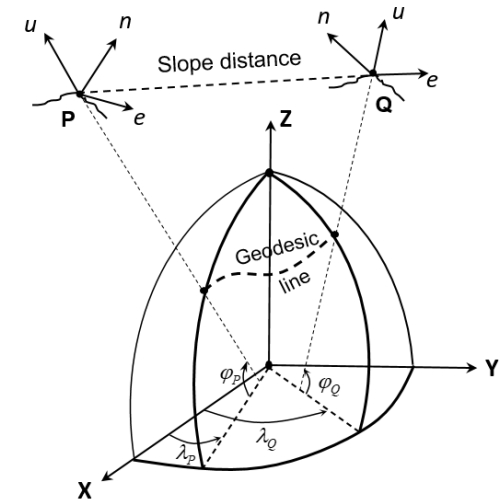
- Average slope angle (reciprocal reading)

$$V_{PQ} = V = 90 - Z$$

$$V_{QP} = -V - \beta$$

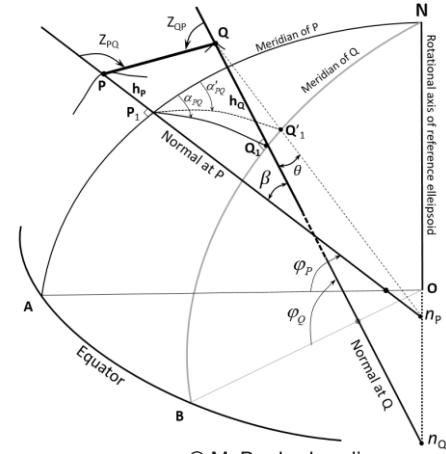
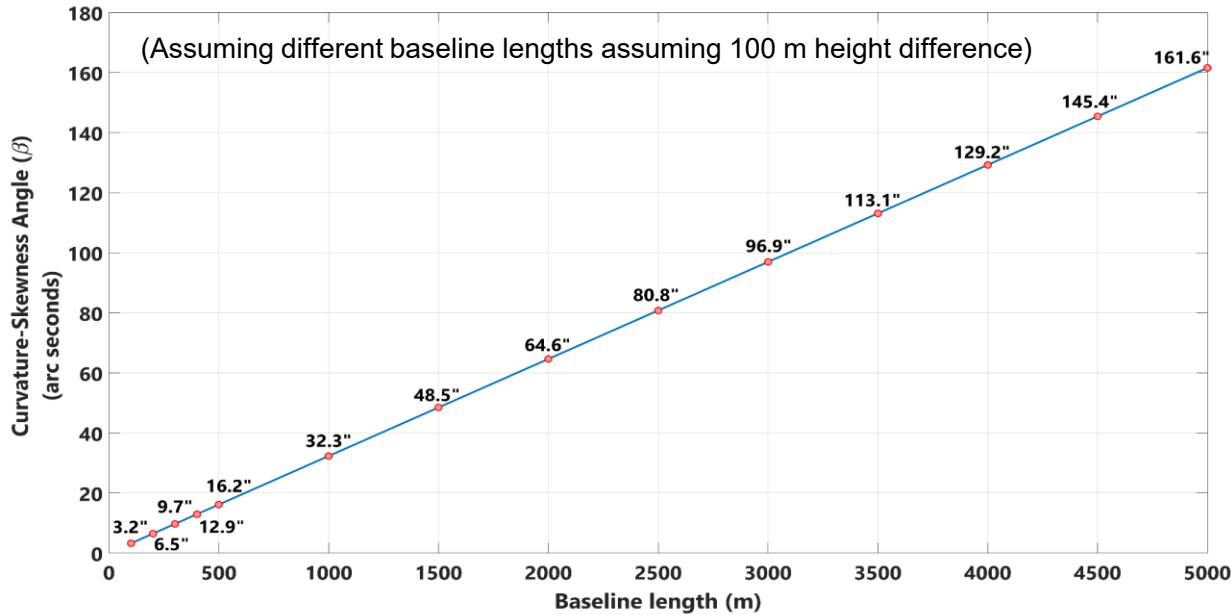
$$\bar{V} = \frac{1}{2}(V_{PQ} - V_{QP}) = V + \frac{\beta}{2}$$

$$\delta_{HD}^{C-S} = SD \cos(V) - SD \cos(\bar{V}) = SD \left[ \cos(V) - \cos\left(V + \frac{\beta}{2}\right) \right]$$





# Angle between normals (curvature-skewness angle)



© M. Bagherbandi  
Sectional view of normal skewness at points P and Q above an ellipsoid of revolution.

Height difference (meter)	Distances (meter)											
	100	300	500	1000	1500	2000	2500	3000	3500	4000	4500	5000
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.4	0.4
5	0.0	0.1	0.2	0.4	0.6	0.8	1.0	1.1	1.3	1.4	1.5	1.6
10	0.1	0.2	0.4	0.8	1.2	1.5	1.9	2.3	2.6	2.9	3.2	3.5
50	0.4	1.2	1.9	3.9	5.9	7.8	9.4	11.7	13.6	15.5	17.3	19.2
100	0.8	2.4	3.9	7.8	11.7	15.6	19.5	23.4	27.3	31.1	34.9	38.8
150	1.2	3.5	5.9	11.8	17.6	23.5	29.3	35.2	41.0	46.8	52.6	58.4
200	1.6	4.7	7.8	15.7	23.5	31.3	39.1	46.9	54.7	62.5	70.2	77.9
250	2.0	5.9	9.8	19.5	29.4	39.1	48.9	58.7	68.4	78.1	87.8	97.5
300	---	---	11.7	23.5	35.2	47.0	58.7	70.4	82.1	93.8	105.5	117.1
400	---	---	15.7	31.3	47.0	62.6	78.3	93.9	109.5	125.1	140.7	156.3
500	---	---	19.6	39.2	58.7	78.3	97.9	117.4	136.9	156.4	175.9	195.4

The curvature-skewness effect on the slope distance reduction in reciprocal measurements.

Unit: mm

The curvature-skewness effect depends on  
**Baseline length**  
**Height difference**

# Is it possible to avoid reading vertical angle and forget the challenges?

Refraction error

Geometric effects (Curvature-skewness)

Physical effects (Deflection of the verticals)



## Network-Aided Reduction of Slope Distances in Small-Scale Geodetic Control Networks

Masoud Shirazian<sup>1</sup>; Mohammad Bagherbandi<sup>2</sup>; and Hamed Karimi<sup>3</sup>

Journal of Surveying Eng., 2021, 147(4): 04021024

- Adjusting the slope distance observations (**unidirectional**) in the form of a 3D free network adjustment
- Computing adjusted coordinates (E N U ) for all network points using the initial values of coordinates of the geodetic control points
- Computing horizontal distances 
$$D_{ij} = \sqrt{(\hat{E}_i - \hat{E}_j)^2 + (\hat{N}_i - \hat{N}_j)^2}$$
- The calculated horizontal distances, along with the horizontal angles or direction observations, are used then in the process of the 2D network in the final free network adjustment

Is it possible to avoid reading vertical angles?

**Answer: YES!**

# Network-Aided Reduction of Slope Distances in Small-Scale Geodetic Control Networks



Damghan reservoir rockfill dam



Mojen reservoir rockfill dam

**Table 1.** Specifications of the dams of the study areas

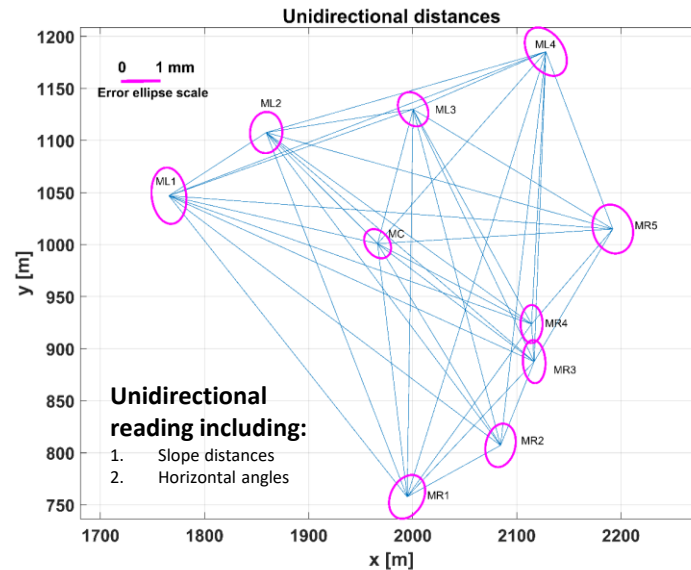
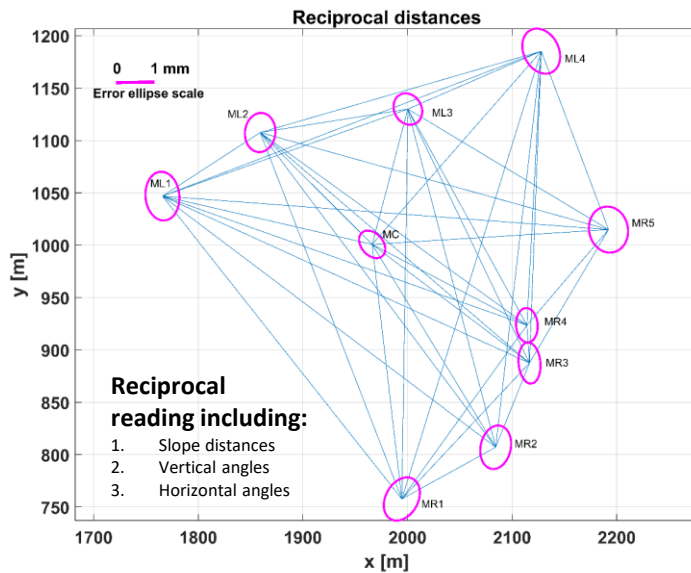
Marker on the map	Name	Dam type	Date of construction	Length (m)	Height (m)
A	Mojen	Rock fill	2018	276	49
B	Damghan	Rock fill	2005	445	54.5

**Table 2.** The data specifications of every observation set

Dam name	Epoch	Date of observation	Instrument used	Distance STD	Horizontal angle STD	Vertical angle STD
Damghan	Epoch no. 2	03/2010	WILD TCA2003	1 mm + 1 ppm	0.5"	0.5"
Mojen	Epoch no. 1	10/2018	WILD T2000 & DI2002	1 mm + 1 ppm	0.5"	0.5"

Note: STD = standard deviation.

# Reciprocal vs unidirectional (network aided) slope distances: Mojen dam

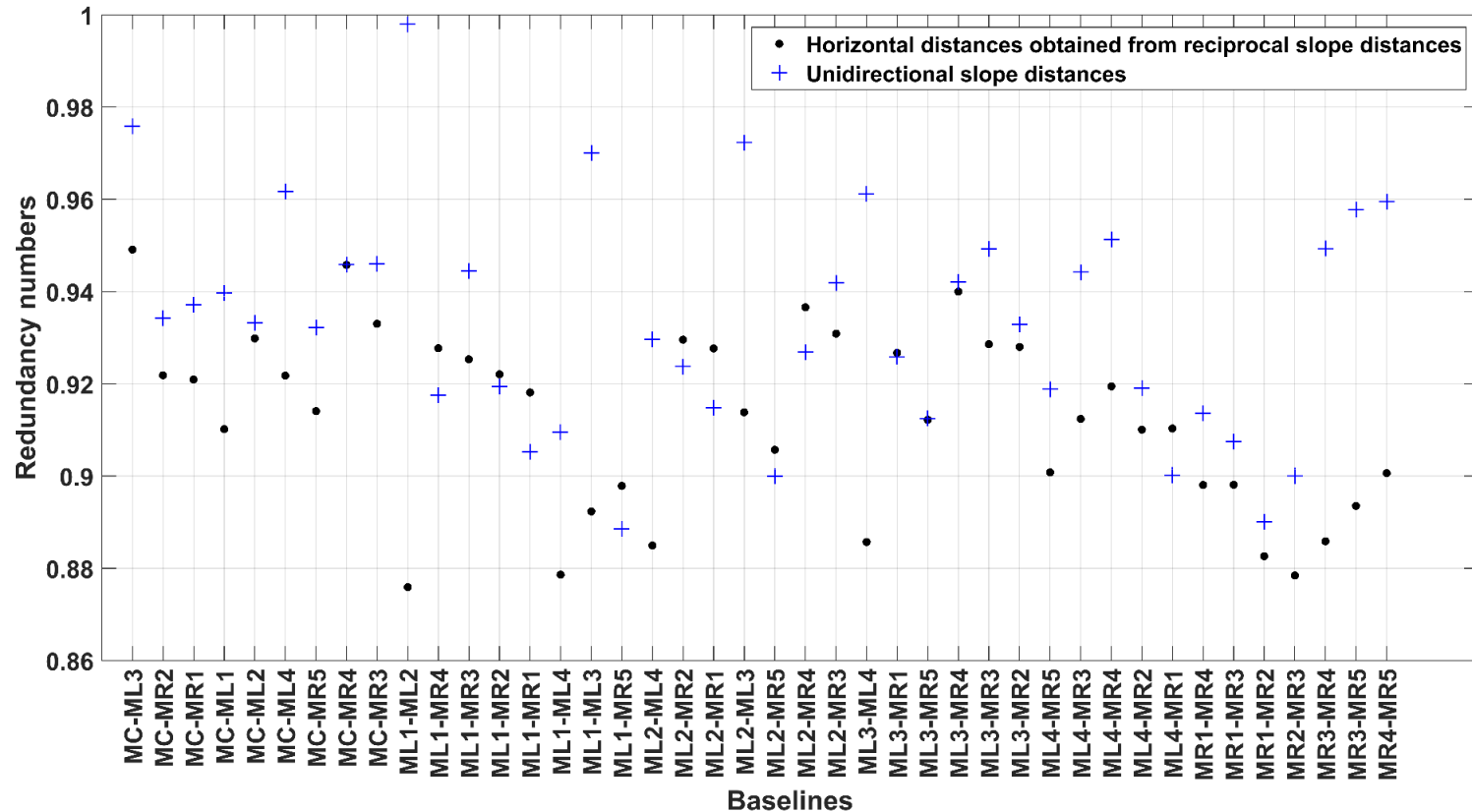


**Table 4.** Comparison of error ellipses and coordinate differences using reciprocal slope distances and unidirectional slope distances in Mojen dam's geodetic control network

Station ID	Using reciprocal slope distances			Using unidirectional slope distances			Difference between coordinates	
	95% semimajor axis (mm)	95% semiminor axis (mm)	Azimuth of major axis (degrees)	95% semimajor axis (mm)	95% semiminor axis (mm)	Azimuth of major axis (degrees)	$\Delta x$ (mm)	$\Delta y$ (mm)
ML1	0.7	0.5	354.7213	0.9	0.5	353.0683	0.2	0.1
ML2	0.6	0.5	6.127042	0.6	0.5	3.861579	0.2	0.3
ML3	0.5	0.4	330.1408	0.6	0.4	328.1169	0.2	0.2
ML4	0.7	0.5	333.4098	0.8	0.5	325.4762	0.6	0.2
MR1	0.7	0.5	29.12523	0.7	0.5	27.69237	0.1	0.2
MR2	0.7	0.5	12.04362	0.7	0.4	12.61253	0.0	0.1
MR3	0.6	0.3	354.7195	0.7	0.3	356.5797	0.3	0.4
MR4	0.5	0.3	356.3522	0.6	0.3	0.426271	0.3	0.5
MR5	0.7	0.6	348.3158	0.8	0.6	342.0895	0.2	0.1
MC	0.5	0.3	318.8208	0.5	0.4	322.8739	0.0	0.1

Note: ID = identification.

# Reciprocal vs unidirectional (network aided) slope distances: Mojen dam



# Take home messages

- The physical and geometric impacts on the vertical angle are important to convert the slope distances to the horizontal ones in the geodetic networks
- One practical solution (according to the surveying guidelines) to eliminate these problems is collecting the vertical angles **reciprocally** and designing the geodetic networks so that the stations' elevations are as much at the **same level** as possible.
  - following the guidelines is sometimes difficult because of the project circumstances
    - establishing a geodetic network for monitoring high towers and structures,
    - existing rough topography.
  - Therefore, designing a geodetic network with all stations **at the same elevation is not always possible**
  - Our results show that ignoring these effects may lead to significant errors, especially if the height differences between the points are large,
    - Even if one measures the vertical angles reciprocally

Take home messages

# Solution: Network-aided method



# For further information



ASCE

## Network-Aided Reduction of Slope Distances in Small-Scale Geodetic Control Networks

Masoud Shirazian<sup>1</sup>; Mohammad Bagherbandi<sup>2</sup>; and Hamed Karimi<sup>3</sup>

**Abstract:** Most of the human-made infrastructures (e.g., dams) need very precise geodetic networks and constant monitoring to detect risks of failure and to plan civil engineering maintenance works. The combination of different measurements helps in determining displacements with high precision; therefore, the risk of damages is reduced. In this paper, we present a new approach, which considers a special geodetic observation strategy as a method to significantly reduce the volume of operations of a precise geodetic network and changes the designing concept of such networks. Decrease in data collection time and cost while keeping or increasing the quality of control networks has been one of the most important goals of any network designer. This paper proposes a method exploiting network properties to convert slope distances to the horizontal ones to be used in the classic terrestrial geodetic two-dimensional (2D) networks. We have evaluated the proposed method in different dam geodetic control networks in Iran. The network adjustment results show the acceptable performance of the presented method compared with the methods that are currently in use. DOI: [10.1061/\(ASCE\)SU.1943-5428.0000375](https://doi.org/10.1061/(ASCE)SU.1943-5428.0000375). © 2021 American Society of Civil Engineers.

**Author keywords:** Control network; Dam deformation; Optimization; Reciprocal reading; Slope distance reduction; Vertical refraction.

ASCE

## Physical and Geometric Effects on the Classical Geodetic Observations in Small-Scale Control Networks

Mohammad Bagherbandi<sup>1</sup>; Masoud Shirazian<sup>2</sup>; Jonas Ågren<sup>3</sup>; and Milan Horemuz<sup>4</sup>

**Abstract:** In classical two-dimensional (2D) geodetic networks, reducing slope distances to horizontal ones is an important task for engineers. These horizontal distances along with horizontal directions are used in 2D geodetic adjustment. The common practice for this reduction is the use of vertical angles to reduce distances using trigonometric rules. However, one faces systematic effects when using vertical angles. These effects are mainly due to refraction, deflection of the vertical (DOV), and the geometric effect of the reference surface (sphere or ellipsoid). To mitigate refraction and DOV effects, one can choose to observe the vertical angles reciprocally if the baseline points' elevation difference is small. This paper quantifies these effects and proposes a proper solution to eliminate the effects in small-scale geodetic networks (where the longest distances are less than 5 km). The goal is to calculate slope distances into horizontal ones appropriately. For this purpose, we used the SWEN17\_RH2000 quasigeoid model (in Sweden) to study the impact of the DOV applying different baseline lengths, azimuths, and vertical angles. Finally, we propose an approach to study the impact of the geometric effect on vertical angles. We illustrate that the DOV and the geometric effects on vertical angles measured reciprocally are significant if the height difference of the start point and endpoint in the baseline is large. Geometric correction should be considered for the measured vertical angles to calculate horizontal distances correctly if the network points are not on the same elevation, even if the vertical angles are measured reciprocally. DOI: [10.1061/\(ASCE\)SU.1943-5428.0000407](https://doi.org/10.1061/(ASCE)SU.1943-5428.0000407). © 2022 American Society of Civil Engineers.

**Author keywords:** Geodetic network; Deflections of the vertical (DOV); Geometric effects; Normal skewness; Refraction; Vertical angle.

**Thank you for your attention!**